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# 1 Electrochemical Impedance Spectroscopy on biofilm electrodes -

# 2 conclusive or euphonious?

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11 Abstract: Electrochemical impedance spectroscopy (EIS) is a versatile tool that is also exploited to 12 study bioelectrochemical systems and biofilm electrodes. EIS can be used to examine characteristics 13 of biofilm electrodes, which are not accessible by direct current measurements like biofilm resistance 14 and biofilm capacitance. EIS in microbial electrochemistry is sometimes applied superficially or 15 evaluation of presented data is not comprehensive due to misinterpretation or missing data validation. 16 This hinders a more widespread application of this method, not only for determination of specific 17 biofilm electrode parameters, but also from a more practical perspective, e.g. as tool for in situ 18 condition monitoring of biofilm electrodes. We discuss how a careful choice of the experimental setup 19 as well as extraordinary diligent EIS data interpretation using electrical equivalent circuit models can 20 lead to conclusive data and meaningful insights. We illustrate the special challenges of studying biofilm 21 electrodes on the example of graphite anodes. We provide an initial guidepost on how to use EIS on 22 biofilm electrodes that requires several preconditions, careful choice of experimental parameters and, 23 nearly mandatory for novices like us, the consultation of experienced operators of EIS.

24

## 25 Keywords

26 Microbial electrochemical technologies, Electroactive microorganisms, Exoelectrogens, Alternating

- 27 current, Biofilm properties.
- 28

#### 29 1. Why using EIS for the study of biofilm electrodes?

30 Microbial electrochemistry has developed from the periphery to the center of bioelectrochemistry. 31 Microbial electrochemistry is the study, engineering and application of interactions of microbial cells 32 with solid electron conductors (electrodes). For the versatile types of interaction please see Schröder et al 2015 [1]. Here we focus on the most-immediate interaction: biofilm electrodes. Biofilm electrodes 33 34 are composed of electroactive microorganisms (EAM) embedded in (their self-produced) matrix of 35 exopolymeric substances (EPS) on the surface of the electrode. The electrode serves either as terminal 36 electron acceptor (biofilm anodes) or as electron donor (biofilm cathodes). Biofilm electrodes are the 37 beating heart of primary microbial electrochemical technologies (MET). MET are a fascinating 38 technology platform [1,2] departing from its archetype the microbial fuel cell (MFC) [3,4] and recently 39 moving towards building electronic circuits based on microbial wires [5]. Using biofilms electrodes in 40 primary MET, e.g. biosensors [6,7], does not only require comprehensive knowledge of their 41 electrochemical and metabolic performance as well as their ecology [8]. It also creates the need of in 42 situ monitoring of physical integrity and functionality [9].

43 Biofilm electrodes are assessed at different hierarchical levels (subcellular – cellular – biofilm) using a 44 whole arsenal of techniques [10]. These include electrochemical methods. Most popular are direct 45 current (DC) methods, e.g. chronoamperometry (CA) and cyclic voltammetry (CV) [11]. Using DC 46 methods always mixtures of non-faradaic current and faradaic current, including pseudo-capacitive 47 currents, e.g. caused by excess electrons stored in the outer membrane cytochromes of Geobacter spp. biofilms, are recorded as well as only the sum of overpotentials. Distinction of different 48 49 overpotentials and their causation, e.g. diffusion, activation or resistance, is highly tedious or even 50 impossible. Electrochemical impedance spectroscopy (EIS) uses alternating current (AC) and thereby 51 enables to obtain properties difficult to determine otherwise [12]. EIS allows to detangle ohmic as well 52 as frequency dependent resistance that is the impedance Z. Furthermore, using EIS the capacitive (ZC) 53 and inductive (ZI) nature as well as diffusion processes (e.g. Warburg impedance ZW) can be 54 examined [13]. Thus, EIS is a helpful method that can provide unprecedented insights into electrode 55 properties. EIS is not only applied, for instance on lithium-ion batteries or fuel cells, but also for 56 biosensing and biofilm electrodes [14,15]. However, its application is not straightforward and needs 57 an experienced operator, but especially knowledge on the electrochemical system under study. This 58 combination seems to be rare when EIS is applied on biofilm electrodes. At the same time, highly 59 valuable work exists that can be used as a foundation for the increased meaningful application of EIS 60 on biofilm electrodes. Here we like to provide an overview on important basics of EIS in general as well 61 as main aspects that specifically have to be considered when applying EIS on biofilm electrodes. Within 62 this article we intend to provide a "guidepost" that helps interested researchers as well as newcomers 63 in the field of EIS to find their way to conclusive application of EIS on biofilm electrodes.

#### 64 2. A brief introduction into EIS and its application on biofilm electrodes

This article solely refers to EIS in the frequency range using potential perturbation. Therefore, a small  $\Delta E$  is applied at a defined frequency range and the current response  $I_t$  is measured. The application of galvanostatic EIS, potential step functions, random signals or advanced EIS measurements in the time domain [16,17] are not subject of this article, as these have not yet been applied on biofilm

69 electrodes to the best of our knowledge.

- EIS is based on recording the current response  $I_t$  to a sinusoidal potential perturbation stimulus  $E_t$ (see also BOX1). The impedance spectrum is obtained by sweeping  $E_t$  at constant  $\Delta E$  through a frequency range, being for biofilm electrodes usually in the mHz to MHz range. Two types of graphs are commonly used to visualise and interpret EIS data [18]. The Nyquist Plot (or Complex Plane Plot, see Figure 1a) shows the imaginary part ( $Z_{Im} = i|Z|sin\varphi$ ) over the real part ( $Z_{Re} = |Z|cos\varphi$ ) of the impedance, whereas the Bode plot (Figure 1b), shows the absolute magnitude of the impedance *IZI*, also called modulus, and the phase shift  $\varphi$  at two different Y-axes over the log<sub>10</sub> of the applied
- 77 frequencies.



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Figure 1: Idealised EIS data of an electrode immersed into an electrolyte with (a) Nyquist plot and (b)
 Bode Plot. The system is modelled with (c) an electrical equivalent circuit with two resistors in series
 and a capacitor in parallel, WE: Working electrode C<sub>dl</sub>: Capacitance of the electrochemical double layer,
 R<sub>pol</sub>: Polarisation resistance of the electrode, R<sub>el</sub>: Electrolyte resistance (the value depends on the
 distance between working electrode and reference electrode), f<sub>ZIm\_max</sub>: frequency at maximum Z<sub>Im</sub> (own
 data, J. Kretzschmar, PhD thesis, 2017).

In the following, we highlight the challenges especially associated to the experimental setup for EIS on biofilm electrodes. Specific data analysis such as model based evaluation of EIS data or data validation can be covered only limitedly and the reader is referred to textbooks [13,18,19] or specific literature, e.g. [20,21]. Evaluation of artefacts in EIS, e.g. caused by induction, are discussed, e.g. by Veal et al. [22].

## 90 BOX1 Basics of Electrochemical Impedance Spectroscopy

91 The Impedance Z can be described analogously to Ohm's law:

92  $Z = \frac{E_t}{I_t} = \frac{\Delta E \sin(2\pi f t)}{\Delta I \sin(2\pi f t + \varphi)}$  Eq. 1 [19]

93 E: potential [V], I: current [A],  $2\pi f = \omega$  = angular velocity [rad s<sup>-1</sup>], t: time [s],  $\varphi$ : phase shift

- 94 [rad] or  $[\circ]$ ,  $E_t$  and  $I_t$  represent E and I as function of time.  $E_t$  is applied as AC potential perturbation
- 95 at constant  $\Delta E$  while  $I_t$  is measured.
- 96 The phase shift  $\varphi$  relates the sinusoidal wave of  $I_t$  and  $E_t$ .  $I_t$  can be leading (being ahead of) or lagging
- 97 (being behind of)  $E_t$  in the phasor diagram. The phase shift  $\varphi$  is depending on the properties of the
- 98 electrochemical system (leading corresponds to capacitance, lagging to inductance). To describe this

- 99 relationship for a sinusoidal AC signal over time, Z needs to be represented as a complex function and
- therefore, consists of a real part ( $Z_{Re}$ ) and an imaginary part ( $Z_{Im}$ ) described by  $i = \sqrt{-1}$  or  $i^2 = -1$ .

# 101 $Z = Z_{Re} - iZ_{Im}$ Eq. 2 [19]

102 Electrical circuit elements being purely imaginary such as capacitors or inductors, show  $\varphi =$ 

- 103  $\pm 90^{\circ} \left( or \pm \frac{\pi}{2} rad \right)$  whereas purely ohmic resistors show  $\varphi = 0$  (only  $Z_{Re}$ ). For capacitive elements,
- e.g., the electrochemical double layer, the phase shift  $\varphi$  between  $E_t$  and  $I_t$  is related to charge storage.
- 105 The most simple example is a capacitor with  $\varphi = +90^{\circ}$ . Here, the capacitor stores charge during half
- the time of one oscillation period of  $E_t$  and releases charge during the other half. To conclude,
- depending on the properties of the electrochemical system,  $I_t$  resulting from  $E_t$  does not only differ in
- 108 terms of the amplitude but also in terms of  $\varphi$ .

## 109 BOX2 Prerequisites for EIS on electroactive biofilms

Meaningful EIS requires i) linearity, ii) time invariance (stability) with iii) guaranteed causality and iv) 110 finiteness of Z for the applied frequencies, f. Linearity means that the relation of the potential 111 112 stimulus and the current answer of the biofilm electrode must be linear and is independent from the 113 amplitude of the stimulus. For electrochemical systems that are usually highly non-linear this is only true for small potential perturbations of  $\Delta E \approx 10 \ mV$  , as  $\Delta E < 10 \ mV$  worsen the signal to noise 114 115 ratio, whereas  $\Delta E > 10 \ mV$  increases the risk to leave the pseudo-linear region. Time invariance 116 means that the systems remains stable until perturbation and returns to its initial state after 117 perturbation. Causality means that the current response of the system is strictly determined by the 118 applied potential perturbation. Finiteness means that there is always a response  $(I_t)$  of the system to 119 the applied stimulus [23]. Biofilm electrodes fulfil these preconditions to a limited extend, as especially

120 time invariance is difficult to achieve over several hours.

## 121 3. Preconditions and consequences for experimentation and data evaluation

EIS on biofilm electrodes follows the same steps like in other fields, that are i) a setting up a suitable experimental system, ii) choice of parameters (e.g.  $\Delta E$  and range of f), iii) data evaluation and iv) data validation [14,23]. In the following, we focus on challenges of EIS measurement being specific for biofilm electrodes. A comprehensive evention on using EIS for MET is given by Yebs at al. [22]

biofilm electrodes. A comprehensive overview on using EIS for MET is given by Yoho et al. [23].

## 126 Experimental setup

127 Electrode size, shape and material have a substantial impact on EIS data. For biofilm electrodes 128 carbonaceous materials are very common due to their biocompatibility, chemical and microbial stability and low price [24]. Unfortunately, carbonaceous materials such as graphite felt or graphite 129 rods possess a high capacitance (~1 mF cm<sup>-2</sup>) as already shown by ter Heijne et al. 2015 [25] that 130 131 influences the accurate determination of biofilm properties such as charge transfer, biofilm and 132 diffusion resistances, and biofilm capacitance as a measure of biofilm thickness or mass [25,26]. The 133 challenge of using graphite electrodes to determine specific biofilm properties is exemplarily shown in Figure 2 a-c. Here, fractions of mature Geobacter spp. dominated biofilm were successively removed 134 from a monolithic graphite anode ( $A = 3.34 \text{ cm}^{-2}$ ) implemented in a flow cell (V = 100mL) while all 135 other parameters remained constant, i.e. temperature, substrate concentration ( $c = 2mmol L^{-1}$ 136 acetate), anode potential ( $E_a = 0.399 V vs. SHE$ ) and stirrer speed (250 rpm). The Nyquist plot 137 (Figure 2 b) and the Bode Plot (Figure 2 c) show results of EIS using  $\Delta E = 10 \ mV$  and a range of f =138

- 139 10 mHz - 10 kHz. It is evident that successive removal of biofilm changes the impedance only to a 140 limited extent. Total biofilm removal, however, may indicate a massive contribution of capacitance of 141 the naked graphite electrode that is shown by the wide opened arc in Figure 2 b. Furthermore, when 142 removing the biofilm partially, capacitance seems to increase due to the increasing diameter of the 143 small arcs in Figure 2 b. This seems counterintuitive, as biofilm capacitance should decrease during 144 biofilm removal. Another explanation might be that without biofilm, the data shows "infinite" charge 145 transfer resistance of the naked graphite electrode. If a biofilm is present, a finite charge transfer 146 resistance is introduced that decreases with increasing biofilm coverage and therefore, a semi-circle
- 147 appears.
- Figure 2 d shows the effect of removal of acetate (sole energy and carbon source) from the electrolyte solution for an electrode fully covered with biofilm compared to an electrode without biofilm. Here, it seems that limiting the metabolism of the biofilms has apparently a similar impact as total removal of the biofilm. This could be a consequence of the dominating capacitance of the graphite electrode,
- 152 changed diffusion regimes or increased charge transfer resistance due to reduced metabolic activity.
- 153 One possible way to overcome, e.g. limitations induced by the capacitance of electrode backbones, is 154 the use of materials with low capacitance but sufficient biocompatibility. Ter Heijne et al. 2018 [26] 155 successfully used Fluorinated Tin Oxide as anode material to identify capacitance of biofilm anodes 156 with up to 450  $\mu$ F cm<sup>-2</sup> as a measure of biofilm growth.
- 157 Mass transport and especially diffusion is also influencing. As often stirring is used to prevent mass 158 transfer limitations in solution, diffusion at and in biofilm electrodes also plays a crucial role when 159 interpreting EIS data [25,27,28]. Noteworthy, from a practical perspective stirring may interfere with 160 the measurement by compromising the causality, e.g., due to induction caused by magnetic stirrers 161 [23]. EIS data displays different types of diffusion: i) semi-infinite linear diffusion that appears as a 45° 162 line in Nyquist plots (i.e. the Warburg impedance ZW), ii) finite space diffusion that appears as 45° line 163 followed by vertical line in low frequency regions and iii) finite length diffusion that appears as 45°line 164 followed by a half circle in low frequency regions of a Nyquist plot, for details please see, e.g. [23,29] 165 (another convenient overview is: Matt Lacey - Battery Science and Electrochemistry, URL: 166 http://lacey.se/science/eis/diffusion-impedance/). Using stirring, EIS data of biofilm electrodes may 167 furthermore show transition from semi-infinite linear diffusion to finite length diffusion. However, 168 using a rotating disc electrode Babauta and Beyenal [27] showed that diffusion in biofilms is only rarely 169 affected by mass transport in solution. To conclude, EIS is very suitable for evaluating mass transfer 170 effects at biofilm electrodes, in biofilms or porous electrodes whereby systematic studies on this topic
- are rare.



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**Figure2:** Effect of biofilm removal from graphite rods and change of substrate concentration for fully intact biofilms on EIS data, (a) scheme of successive biofilm removal with pink parts showing biofilm and grey parts showing the graphite electrode, (b) Nyquist Plot and (c) Bode Plot of successively removing *Geobacter* spp. dominated biofilms at constant substrate concentration (2 mmol L<sup>-1</sup> acetate), (d) combination of complete biofilm removal and complete substrate (acetate) removal at fully intact *Geobacter* spp. dominated biofilm electrodes, red data in (c) and (d) shows phase shift  $\varphi$  of  $I_t$ . (own data, J. Kretzschmar, PhD thesis, 2017).

#### 180 **3.1. Choice of parameters**

EIS on biofilm electrodes is mostly performed with a potential perturbation at a set electrode potential to sustain metabolic activity of the EAM. EIS at open cell potential (OCP) is also possible, but bares the risk of instability that is losing time invariance. It is very difficult and takes at least hours to achieve steady state conditions at OCP for *Geobacter* spp. dominated biofilm anodes.

185 Generally,  $\Delta E$  between 10 -20 mV has been shown as suitable [23]. The frequency range defines the 186 duration of the measurement and hence, has a direct influence on achieving time invariance. This is of 187 special notice for measurements at OCP as well as biofilm electrodes facing non-constant substrate 188 concentration or substrate limiting conditions, e.g. in batch operation. Consequently, EIS on biofilm 189 electrodes should be limited to small frequency ranges and frequencies higher than 10 mHz. Careful 190 data validation (see paragraph 3.3) is required to assure time invariance as well as linearity and 191 causality.

## 192 **3.2. Model based evaluation**

EIS is analysed by fitting the acquired data to a mathematical model of an electrical equivalent circuit (EEC) describing electrochemical processes in the system under observation. EEC models consist of a limited number of electric circuit elements including capacitors and resistors as well as diffusion processes and others [19,21,23]. This is challenging, especially when examining porous biofilm electrodes in stirred experimental setups. Increasing the number of EES elements may improve the fit but not the understanding of the system and it also increases the challenge of model validation. Therefore, we need to differentiate two cases where EIS on biofilm electrodes can be applied. The first case is application of EIS to improve mechanistic understanding of electrochemical processes in biofilm electrodes. The second case is to use EIS as a tool for rather simple condition monitoring of biofilm electrodes, e.g. for sensors.

203 In the first case the prime option is using "white box models" that rely on validated physical equations 204 of the examined electrochemical system. This is challenging for biofilm electrodes due to unknown 205 constants and manifold functional dependencies and needs careful design of the experimental setup, 206 as exemplarily shown in [26]. Several EEC models have been proposed for analysis of EIS data of biofilm 207 electrodes, see e.g. [15,21,26]. Yet, these differ significantly and there is no "gold standard" that is 208 generally applicable due to the heterogeneities of the experimental setups and biofilms. Therefore, it 209 is of high importance to always publish the used EEC model to enable the verification of presented data. The values derived from EEC elements with direct physical meaning, e.g. resistor ( $Z = R = \frac{E}{I}$ ) or 210 capacitor ( $Z_c = \frac{1}{i\omega C}$ ) are relatively easy to interpret. Versatile EEC elements such as the CPE ( $Z_{CPE} =$ 211  $\frac{1}{(i\omega)^{\alpha}A_{CPE}}$ ) may enable fitting but have to be used with great care. The CPE parameters A and  $\alpha$  are 212 frequency independent constants. If lpha=1,A represents a pure capacitor with  $arphi=-90^\circ$ . For lpha=0213 214 the CPE represents a resistor with  $\varphi = 0^{\circ}$  and for  $\alpha = -1$  an inductor with  $\varphi = 90^{\circ}$  [21]. Furthermore, semi-infinite linear diffusion can be described with a CPE using  $\varphi = 45^{\circ}$  or  $\alpha = 0.5$ . This makes the 215 216 CPE a versatile element. However, fitting the CPE in an EEC without further information may not allow 217 to unravel detailed physical-chemical characteristics of the underlying processes. This disadvantage 218 turns into an advantage in the second case, where EIS is applied for condition monitoring of biofilm 219 electrodes. Here, the intention is not to decipher specific electrochemical processes but changes of 220 these processes and therefore allows to apply CPE in rather unspecific "grey box models". Grey box 221 models are easier to develop and still allow determination of structural or functional changes of the 222 biofilm electrode such as the biofilm integrity (see Figure 2). Nevertheless, they are only applicable to 223 one specific setup and do not reveal specific numbers of, e.g. diffusion constants, resistance or 224 capacitance.

#### 225 3.3. Data validation

226 When using EIS it is crucial to prove linearity, causality and stability of the system under observation 227 (see BOX 2). The Kramers-Kronig (K-K) relation is used by default for validation of EIS data 228 [13,23,30,31]. The K-K relation is the mathematical proof that the studied system fulfils the four 229 requirements of EIS by calculating  $Z_{Re}$  from  $Z_{Im}$  and vice versa. There exist several methods to carry 230 out K-K transformation in practice, some are described in [18]. Usually, software for EIS also contains 231 a K-K function for data validation. However, K–K transforms are only mathematical results that do not

reflect the real physical properties of the system [13] and are also sensitive for stochastic errors [18].

233 A much simpler but more robust alternative to the K-K transform is to perform a forward as well as

backward scan of the applied range of *f*, meaning performing EIS from high to low and from low to

high frequencies. Validity is confirmed in first approximation, if the results of the both scans are

- 236 identical. Unfortunately, K-K transforms, simple frequency scans and even simple replicates are rarely
- 237 reported for EIS on biofilm electrodes making it difficult to verify the published data.

#### 238 4. Conclusions

239 EIS can be a valuable tool to study biofilm electrodes providing advantages over common DC methods. 240 Several pitfalls during application of EIS on biofilm electrodes and data evaluation define the need of 241 careful design of the experimental setup in order to avoid interference, e.g. by the electrode material (capacitance) or stirring (diffusion). Furthermore, definition of measurement parameters such as 242 243 frequency range and electrode potential need care to assure linearity and stability. Here, frequency 244 range, amplitude of the perturbation signal and applied electrode potential are of specific interest, as 245 e.g. measurements at OCP requires time and careful experimentation to achieve steady state. Finally, we highly recommend performing validation of EIS data of biofilm electrodes. It is a necessity to 246 247 improve and enhance the meaningful application of EIS in microbial electrochemistry. EIS allows to 248 derive parameters such as biofilm capacitance, charge transfer resistance or diffusion at biofilm 249 electrodes or in-situ monitoring of the biofilm integrity. For the latter it is worth to evaluate the 250 applicability of grey box models or the use of indirect or contactless EIS for biofilm characterization as 251 shown by Turick et al. [32]. Finally, we encourage to consider using EIS in a meaningful way to evaluate 252 biofilm electrodes or MET in general, e.g. for monitoring membrane fouling [33].

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