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Mechanisms of heating-electrokinetic co-driven perfluorooctanoic acid (PFOA) adsorption on zeolite Yongping Shan^{1,4}, Yuzhou Yin¹, Jian Wei², Dong Ma¹, Mingxiu Zhan^{1,3}, Yongguang Yin¹, Liuqing Yang¹, Wentao Jiao^{1*}, and Lukas Y. Wick⁴ ¹ Research Center for Eco-Environmental Sciences, Chinese Academy of Sciences, 100085 Beijing, China. Email: ypshan@rcees.ac.cn ² State Key Laboratory of Environmental Criteria and Risk Assessment, Chinese Research Academy of Environmental Sciences, Beijing 100012, China. ³ College of Metrology and Measurement Engineering, China Jiliang University, Hangzhou 310018, Zhejiang, China. ⁴UFZ - Helmholtz Centre for Environmental Research, Department of Environmental Microbiology, 04318 Leipzig, Germany. *Corresponding author: E-mail: wtjiao@rcees.ac.cn (W. Jiao).

Abstract: Slow release of emerging contaminants limits their accessibility from soil to pore water, constraining the treatment efficiency of physio-chemical treatment sites. DC fields mobilize organic contaminants and influence their interactions with geo-matrices such as zeolites. Poor knowledge, however, exists on the joint application of heating and electrokinetic approaches on perfluorooctanoic acid (PFOA) transport in porous media. Here, we investigated electrokinetic PFOA transport in zeolite-filled percolation columns at varying temperatures. Variations of pseudo-second-order kinetic constants (k_{PSO}) were correlated to the liquid viscosity variations (η) and electroosmotic flow velocities (v_{EOF}). Applying DC fields and elevated temperature significantly (>37%) decreased PFOA sorption to zeolite. A good correlation between η , v_{EOF} , and k_{PSO} was found and used to develop an approach interlinking the three parameters to predict the joint effects of DC fields and temperature on PFOA sorption kinetics. These findings may give rise to future applications for better tailoring PFOA transport in environmental biotechnology.

47 Keywords

48 PFOA; emerging contaminant; electrokinetic; temperature; sorption kinetics;

49 1. Introduction

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50 Persistent toxic perfluorooctanoic acid (PFOA) has been detected worldwide (Flores et al., 2013; Lein et al., 2008; Lindim et al., 2015; Lorber et al., 2015), threatening the health of 51 52 aquatic living, animals, and humans (Benninghoff et al., 2012; Hoffman et al., 2010; Jeon et al., 2010; Tsang et al., 2013). Although sorption and permeable reactive barrier (Qian et 53 al., 2022) efficiently remove PFOA from the soil pore water, the slow release of PFOA 54 from contaminated sites to pore water is prolonging and challenging risk management 55 (Cousins et al., 2022). There is hence interest in reducing PFOA sorption from soil, to 56 shorten the release period, especially for the high-concentration point-source soil 57 58 contamination sites.

Sorption reduction in kinetics is governed by the bulk transport, film transport, and intraparticle transport steps (Tran et al., 2017), which may be regulated by electrokinetic and heating approaches. Electrokinetic phenomena are induced by external direct current (DC) electric fields allowing for the directional movement of charged particles in the electrolyte. They include the electrophoresis of charged colloidal particles (Shan et al., 2020a, 2018), the electro-migration of ions (Hunter, 2013; Sprocati and Rolle, 2022), and the electroosmotic flow of liquid (EOF). Electrokinetic technology is commonly used to clean contaminated soil sites, with the combination of surfactants, heating, etc (Ganbat et al., 2022; Niarchos et al., 2022; Wen et al., 2021). EOF, as the surface charge-driven movement of pore fluids (Elimelech et al., 1995) that can mobilize electrically neutral organic contaminants and, thereby influence their interactions with sorbents (Shan et al., 2020b). It originates from the electrical double layer in sorbent pores, and, hence, is thought to efficiently control the liquid flow in the pore networks of sorbents (Shi et al., 2008) and thereby the distribution of chemicals in the nano-size pores (Sprocati and Rolle, 2022). The electroosmotic flow velocity (v_{EOF}) is driven by the surface charge of the solid surface, the electrical double layer thickness, the width of the capillary or pore width, and the liquid viscosity (Lee et al., 2016; Probstein, 1994). And has a plug-shaped velocity profile (Grimes et al., 2000; Kar et al., 2016; Lee and Keh, 2014; Rice and Whitehead, n.d.) that allows for efficient water movement at distances as low as a few nanometers above a sorbent surface. It has been found to reduce the sorption of electrically neutral oil

- 79 contaminant phenanthrene (PHE) in geo-sorbents (silica, zeolite, and Al₂O₃) (Shan et al.,
- 2020b) or to increase dissolution and release of alginate-embedded solid PHE by 120-times
- as compared to stagnant water conditions (Shi et al., 2008).
- 82 Temperature is another driver of the chemical sorption capacity of sorbents and the kinetics
- of chemical sorption to sorbents, respectively (Do, 1998). The sorption capacity describes
- 84 the temperature-dependent equilibrium loading of adsorbate to sorbents and is often
- approximated by Langmuir and Freundlich sorption models (Do, 1998). The sorption
- 86 kinetics reflects the sorption rate over time and is commonly described by kinetic sorption
- 87 models, including the intra-particle model, the pseudo-first-order (PFO), and the pseudo-
- second-order (PSO) model (Kopinke et al., 2018; Tran et al., 2017). Finally, temperature
- also influences the viscosity (η) as a further driver of chemical diffusion and electroosmotic
- 90 flow velocity (Ghosal, 2004).
- 91 Poor knowledge however exists on the joint application of heating and electrokinetic
- 92 approaches on PFOA transport and sorption in porous media. With a pKa of 0-1 (Goss,
- 93 2008), PFOA will be predominantly deprotonated at neutral pH. Electrokinetic PFOA
- 94 transport and sorption thus will be driven by EOF, sorption strength, and environmental
- 95 conditions such as temperature. Here, we investigated electrokinetic PFOA transport in
- 26 zeolite-filled percolation columns at pH = 7, yet varying temperatures, calculated PFOA
- 97 pseudo-second-order (PSO) kinetic constants (k_{PSO}) of PFOA sorption to zeolite and
- orrelated them to viscosity changes (η) and calculated EOF velocities (ν_{EOF}). We also
- 99 addressed the following questions: i) what are the effects of DC electric fields and
- temperature on the transport and sorption of PFOA to zeolites? (ii) what are the driving
- factors of possible synergetic effects? and (iii) can the effects be predicted?

2. Material and Methods

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2.1 Reagents and sorbents

- Perfluorooctanoic acid (PFOA, Sigma-Aldrich, USA) was diluted with DI water to prepare
- the storage solution for sorption experiments. PFOA standard (100 µg/mL in MeOH) (J&K
- Scientific, Germany) was diluted with ultrapure water for LC-MS/MS measurements.

- Potassium dihydrogen phosphate and dipotassium hydrogen phosphate (Macklin, USA),
- were diluted in DI water to prepare a 100 mmol/L phosphate buffer (PB, pH=7.0). The
- specific surface area and average pore width distribution of zeolite (Si:Al = 2.5:1, Macklin,
- 110 USA) were determined by a specific surface area and pore width analyzer (ASAP2460,
- McMurraytec, USA) (Appendix A **Table S1**), the zeta potential of zeolite in 100 mM PB
- 112 (pH=7.0) was determined by a zeta potential analyzer (ZS90, Malvern, UK) with disposal
- 113 folded capillary cells.

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2.2 Analytical methods

- 115 PFOA was quantified by a LC-MS/MS system (6460 and 1290 Infinity, Agilent, USA),
- using a C18 column, (ZOBRAX RR Eclipse Plus, Agilent, USA). Methanol and 10 mmol/L
- ammonium acetate were mixed as the mobile phase, following a time-dependent gradient
- as listed in Appendix A **Table S2**. Multiple reaction monitoring and electron spray
- ionization modes were adopted to quantify PFOA. Calibration curves (0.01-0.1, 0.1-1.0,
- and 1.0-10 mg/L, cf. Appendix A Fig. S1) were established at the beginning of each
- measurement batch with standards, batch samples ≤ 50 and $R^2 \geq 0.999$ were required to
- 122 control data quality.

2.3 Kinetics of PFOA sorption in percolation systems

- 124 Electrokinetic percolation columns adopted from our previous work (Shan et al., 2018)
- were settled in a water bath with temperature-conditioning (DLSB 5L/10, Yuhua, China)
- for kinetic experiments (Appendix A Fig. S2). Zeolite was washed 3 times with de-ionized
- water and dried for 12 h at 80°C in the oven and kept in a vacuum desiccator till use. The
- electrokinetic apparatus was wet-packed with 6 g zeolite in PB. Two disc-shaped Ti/Ir
- electrodes at the top (cathode) and bottom (anode) of the column were connected to a DC
- power pack (IT6720, Itech, China) to produce electric field strengths X = 1, 2, and 3 V/cm,
- resulting in stable direct currents of 0.03 A, 0.06 A, and 0.09 A, respectively. Then 10 mg/L
- 132 PFOA in PB electrolyte was pumped through the column under static temperatures of 10,
- 133 20, 30, 40, and 50 □ with deviations \le 2°C. 1 mL liquid was sampled before and after
- percolation at given time intervals up to 48 hr. After centrifugation at 5000 x g, the
- supernatant was measured with LC-MS/MS. Each experiment was conducted in triplicate.

Breakthrough curves and the mass of PFOA accumulating on zeolite under varying DC electric field strengths and temperatures can be depicted by the PFOA concentration shifting over sorption time.

2.4 Isotherm PFOA sorption experiments

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Isotherm batch experiments were conducted in PB in sealed 15 mL polypropylene centrifuge tubes at a sorbent-to-liquid ratio of 1:1000 (g/mL), with 8 initial PFOA concentrations ranging from 1 to 8 mg/L. Zeolite and liquids in the centrifuge tubes were equilibrated in a horizontal shaker with temperature conditioning (HNYC-211C, Ounuo, China) at 150 r/min for 7 days at temperatures of 10 °C, 20 °C, 30 °C, 40 °C, and 50 °C, with fluctuations < 2 °C. Zeolite particles were ground into a fine powder with an average particle diameter of $74 \pm 4 \,\mu m$ to shorten the equilibrium time, the powder zeolite was only used in isothermal experiments. After equilibrating for 7 days, liquid-zeolite suspensions were centrifuged at $5000 \times g$ for 10 min, 1 mL samples were taken by a syringe gently from the supernatant and measured by LC-MS/MS. Each experiment was conducted in triplicate.

2.5 Calculation of EOF velocities

EOF velocity (v_{EOF}) in a pore of radius r (Vallano and Remcho, 2000) was quantified by the maximum v_{EOF} ($v_{EOF,max}$) and a function ($f(\kappa r)$), which includes electrical double layer and pore radius effects (Rice and Whitehead, 1965) (eqs. 1-3)

$$v_{EOF} = v_{EOF, \max} * f(\kappa r)$$
 (1)

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$$v_{EOF, \max} = -\frac{\varepsilon_r \varepsilon_0 X \xi}{\eta}$$
 (2)

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$$f(\kappa r) = \left(1 - \frac{2I_1(\kappa r)}{\kappa r I_0(\kappa r)}\right)$$
 (3)

where I_0 is the modified Bessel function zero order, I_1 is the modified Bessel function of the first order, κ is the reciprocal of the electrical double layer thickness (1/m) (Sharma and Hanumantha Rao, 2003), and r is the intra-particle pore radius of zeolite (m). ε_r is the dielectric constant, ε_0 is the vacuum permittivity (F/m), η is the liquid viscosity (Pa s), ξ is the zeta potential of zeolite (V), and X is the DC field strength (V/m).

2.6 Kinetic and isotherm models

164 2.6.1. Kinetic equations

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- Sorption kinetic is the rate of PFOA adsorbed onto zeolite. It can be analyzed by
- mathematical models including the intra-particle model (eq. 4), the pseudo-first-order
- 167 (PFO) model (eq. 5), and the pseudo-second-order (PSO) model (eq. 6).
- 168 The linearized expression of the intra-particle diffusion model (Lei et al., 2022) is

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$$q_t = k_n t^{1/2} + C \tag{4}$$

- where k_p (mg/g/min^{1/2}) is the kinetic constant of the intra-particle diffusion model and C
- 171 (mg/g) is a constant.
- In the PFO model (Yu et al., 2009) the q_e and q_t are the adsorbate concentration in the
- sorbent at equilibrium and at time t (1/hr), respectively; k_{PFO} is the kinetic constant.

$$\ln(q_e - q_t) = -k_{PFO}t + \ln q_e$$
 (5)

- 175 The PSO model can be described by the equation with k_{PSO} being the PSO kinetic constant
- 176 (g/mg/hr).

$$\frac{t}{q_t} = \left(\frac{1}{q_e}\right)t + \frac{1}{k_{\rm PSO}q_e^2} \tag{6}$$

178 2.6.2. Isotherm equations

- 179 Sorption isotherms describe the relationship between the amount of PFOA adsorbed onto
- zeolite and the concentration of the adsorbate in the liquid at a constant temperature.
- Sorption isotherms were analyzed by the Freundlich model and the Langmuir model (Tran
- et al., 2017). The Langmuir approach can be described by the equation

$$q_e = \frac{Q_{\text{max}} K_L C_e}{1 + K_L C_e} \tag{7}$$

- where Q_{max} is the max sorption capacity at sorption equilibrium, K_{L} is the Langmuir
- constant, C_e is the PFOA concentration in liquid (mg/L). The Freundlich model is described
- by eq. 8, where K_F refers to the Freundlich constant $((mg/g)/(mg/L)^n)$.

$$q_e = K_F C_e^{\ n} \tag{8}$$

3. Results and Discussion

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3.1 Electrokinetic and temperature effects on PFOA sorption to zeolite

Heating and electrokinetics both decreased PFOA sorption on zeolite. Cumulative PFOA 190 191 mass thereby showed a bi-phasic behavior with a fast initial increase until ca. t = 14 hr 192 followed by reduced mass accumulation increment rate thereafter (Fig. 1). In the absence of DC, heating from 10 °C to 50 °C decreased PFOA loading from 10.1 mg to 7.6 mg (≈25%) 193 reduction) at t = 48 hr. A similar trend was found in the presence of DC, where heating 194 195 from 10 °C to 50 °C decreased sorbed PFOA mass at all electric field strengths applied; e.g., after 48 hr at X = 1 V/cm from 9.4 mg to 7.4 mg (21%), at X = 2 V/cm from 8.7 mg to 196 7.2 mg (17%) at X = 2 V/cm, and at X = 3 V/cm from 8.1 mg to 6.7 mg (17%). At any 197 198 temperature tested, the application of DC fields likewise decreased PFOA loading to zeolite; for instance, after 48 hr at X = 3 V/cm by 20% at 10 °C, 15% at 20 °C, 15% at 30°C, 14% 199 200 at 40 °C, and 12% at 50 °C, respectively. Although PFOA may mostly be ionized (Goss, n.d.) at pH = 7, observed electrokinetic effects on PFOA sorption are in accordance with 201 202 previous research on non-ionic phenanthrene sorption on mineral sorbents revealing 203 reduced v_{EOF} -dependent phenanthrene sorption to zeolites in presence of DC electric fields 204 (Shan et al., 2020b). This shows that electrokinetic phenomena have reduced the availability of PFOA molecules to e.g., intraparticle zeolite sorption sites. The good 205 206 correlation of the observed effects to v_{EOF} further suggests that EOF is a good predictor for electrokinetic sorption effects of anionic ambiphilic compounds such as PFOA where 207 208 interactions of the hydrophobic fluorocarbon part may drive its sorption rates (Yu et al., 209 2009). Our study further extends our knowledge on the effect of temperature on electrokinetic effects on contaminant sorption⁴⁶ and, hence, allows us to apply heating and 210 211 electrokinetic phenomena as drivers for contaminant sorption in future technological applications. 212

3.2 Electrokinetic and temperature effects on PFOA sorption kinetics

Sorption kinetics were further analyzed by fitting the time-dependent sorption data to the pseudo-first-order (PFO), intra-particle diffusion and pseudo-second-order (PSO) models (Ho et al., 2000; Morelis and van Noort, 2008). The regression correlations proposed the

- PSO model to better describe sorption kinetics ($R^2 \ge 0.96$) than the PFO model
- 218 $(0.89 < R^2 < 0.99)$ or the intra-particle model $(0.74 < R^2 < 0.91)$ (Fig. 2, Table 1, Appendix A
- Tables S3 & S4). The kinetic constant of PSO (k_{PSO}) hence enabled us to compare PFOA
- 220 sorption kinetics at the different temperatures and electrokinetic conditions tested.
- Increasing k_{PSO} (10⁻³ g_{zeolite}/mg_{PFOA}/h) thereby points at decreasing PFOA mass sorbing.
- Heating from 10 to 50 °C in the absence of DC increased the k_{PSO} from 256 *10⁻³ g/mg/hr
- 223 to 920 *10⁻³ g/mg/hr (259%) in the absence of electric fields. In presence of DC, k_{PSO}
- 224 increased between 10 °C and 50 °C by 143% (X = 1 V/cm), 91% (X = 2 V/cm), and 42%
- 225 (X = 3 V/cm) (Fig. 2, Table 1, Appendix A S3,). Observed temperature-induced increases
- of k_{PSO} at a given electric field strength were lower at X = 3 V/cm (25%) than at X = 2 V/cm
- 227 (59%), X = 1 V/cm (99%), and X = 0 V/cm (218%) (**Fig. 2, Table 1**, Appendix A **Fig. S3**,
- 228 Tables S3 & S4).
- Both heating and DC electric fields hence resulted in increased k_{PSO} , i.e., reduced PFOA
- sorption and enhanced PFOA transport, respectively (Fig. 3, Appendix A Fig. S4). The
- 231 kinetic model analysis developed our previous work from a time point analysis to the
- sorption kinetics over 48 hr. It also provided an appropriate parameter to quantitatively
- 233 depict electrokinetic effects on sorption kinetics and enabled comparisons between the
- heating effect and the electrokinetic effects over time shifting (Qin et al., 2015; Shan et al.,
- 235 2020b).

3.3 Synergism of electrokinetic and heating effects on PFOA sorption

- Our data propose that electrokinetic transport phenomena at the liquid-sorbent interface
- 238 may influence sorption kinetics. The v_{EOF} has been discussed to be key to DC field effects
- on the sorption of non-ionic phenanthrene at room temperature (Shan et al., 2020b). We
- 240 here further studied drivers of DC field effects at different temperatures on anionic, yet
- partially hydrophobic PFOA. To do so, we first quantified v_{EOF} in intra-particle pores of
- 242 zeolite under various temperatures and DC field strengths by equations 5-7, using
- 243 experimentally determined average pore width, and zeta potential of the zeolite sorbent.
- The temperature-controlled sorption capacity was investigated by the sorption equilibrium
- experiments, and analyzed by Freundlich and Langmuir equations (egs. 7-8). Calculated
- 246 v_{EOF} and isothermal parameters K_F and K_L were subsequently correlated to the

experimentally derived kinetic constants (k_{PSO}).

Regression correlation showed that the $v_{\rm EOF}$ and the $k_{\rm PSO}$ were highly linearly correlated at all temperatures, with $R^2 > 0.96$ (**Fig. 4A**, Appendix A **Table S5**), suggesting that EOF was an apparent driver for observed PFOA sorption kinetic variations. The slope values were positive, indicating that increasing $v_{\rm EOF}$ resulted in higher $k_{\rm PSO}$, and, subsequently, decreased PFOA sorption to zeolite in DC fields. DC effects thereby were significantly (>500%) higher at 10°C as compared to 50°C (**Table 2, Fig. 4A**) indicating the synergetic effects of heating and DC fields on PFOA sorption rates (**Fig. 4B**).

Linking the slope values (derived from linear v_{EOF} - k_{PSO} fitting) with either the Langmuir or Freundlich parameters showed a positive apparent quadratic correlation with $R^2 = 0.996$ for K_L and 0.955 for K_F (**Fig. 4B**). This suggests that K_L may be used to estimate temperature DC-temperature effects on PFOA sorption on zeolites. Decreasing K_L at higher temperatures thus promotes DC field effects on PFOA sorption to zeolite; i.e. a combination of high temperature and high DC field strength leads to less sorption and higher PFOA transport. Such observation is in line with previous research revealing that heating varies the sorption capacity, which in turn may also affect the sorption kinetics(Qu et al., 2009; Yang et al., 2018).

Based on the apparent correlations, we further developed an approach to describe and predict the temperature-dependent electrokinetic effects on PFOA sorption. The approach combines v_{EOF} (as a factor reflecting the presence of DC electric field), liquid viscosity (as a factor reflecting the influence of temperature), and their joint impact on the kinetic constant k_{PSO} (Fig. 5). At low liquid viscosity (e.g. at lower T) and high v_{EOF} (e.g. at elevated X) strongly reduced PFOA sorption, i.e. enhanced PFOA transport through zeolite is evidenced. By contrast, at high viscosity and low v_{EOF} , poor PFOA through zeolite is calculated. Such temperature (i.e. liquid viscosity) dependent correlation extends previous approaches to compare DC field effects on the sorption of a hydrophobic contaminant (phenanthrene) to geo-sorbents(Shan et al., 2020b). Although PFOA in our system may be mobilized both by electromigration and EOF, it further reveals that v_{EOF} nevertheless may be a good descriptor for DC field effects on PFOA sorption and transport in the geo-sorbent zeolite.

3.4 Relevance for environmental and biotechnological applications

Our results reveal that temperature and electrokinetic effects control the sorption kinetics and concomitant transport of PFOA in the geo-sorbent zeolite. Electrokinetic techniques hence may be promising to regulate PFOA-sorbent interactions. Our approach may also be used to kinetically regulate the interaction of other contaminants and zeolite-like sorbents in the manmade/natural environmental (bio-)technology (Qin et al., 2015; Shan et al., 2018). Enhanced PFOA transport may reduce time and subsequent costs of physicalchemical removal processes (e.g., permeable reactive barrier) around point source pollution sites (Ma et al., 2022; Shojaei et al., 2021). As sorption effects in DC fields are temperature dependent, our data further suggest that both the electric field strength and/or the temperature of a given system can be adjusted to the transport needs for PFOA. In summer, for instance, higher environmental temperatures may require lower DC field strengths as in winter, where moderate heating may promote PFOA transport rates. Soil matrices typically consist of a mixture of mineral and carbonaceous materials (Gill et al., 2014; Wick et al., 2007), considering previously investigated mechanisms of electrokinetic-controlled phenanthrene sorption on several carbonaceous sorbents (Qin et al., 2015; Shan et al., 2020b), the temperature-controlled electrokinetic approaches may enhance both hydrophobic and hydrophilic chemical transport through mineral contents in the soil. Such an approach may also elevate the transport, of a wide range of other similar contaminants in zeolite-type geo-matrices, thereby promoting efficient transport to treatment zones and so reducing the threat to the environment and human health. This may give rise to future technical applications, which allow regulating sorption processes, for instance in response to fluctuating adsorbate concentrations in contaminated water streams, in electrobioremediation, or to avoid unwanted sorption solutes in technical applications.

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Appendix A. Supplementary data

- 306 Supplementary data associated with this article can be found in the online version at
- 307 xxxxxxx.

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Table 1. Kinetic parameters of the pseudo-second-order model at temperatures 10 - 50°C and DC field strengths 0 - 3 V/cm.

Temperature	Pseudo-second-order parameters no DC			Pseudo-second-order parameters X = 1 V/cm			Pseudo-second-order parameters X = 2 V/cm			Pseudo-second-order parameters X = 3 V/cm		
(°C)	$q_{ m e}$	k _{PSO} (10 ⁻³ g/mg/hr)	R^2	$q_{ m e}$	k _{PSO} (10 ⁻³ g/mg/hr)	R^2	$q_{ m e}$	k _{PSO} (10 ⁻³ g/mg/hr)	R^2	$q_{ m e}$	k _{PSO} (10 ⁻³ g/mg/hr)	R^2
10	0.35	256	0.98	0.29	401	0.98	0.24	573	0.98	0.21	815	0.9 8
20	0.28	426	0.98	0.24	563	0.98	0.22	735	0.98	0.20	845	0.9 8
30	0.25	547	0.98	0.22	704	0.98	0.20	853	0.98	0.18	1087	0.9 9
40	0.22	709	0.98	0.20	834	0.99	0.19	946	0.99	0.17	1129	0.9 9
50	0.20	920	0.98	0.19	975	0.99	0.18	1096	0.99	0.17	1154	0.9 9

Table 2. Regression results of isothermal and slopes of electroosmotic flow velocity (v_{EOF}) to the kinetic constant (k_{PSO}).

T	Slope	Freundlich param		Langmuir Isotherm parameters			
(°C)	S	$K_{\rm F}$ (mg/g)/(mg/L) ⁿ	n	R^2	q _m (mg/g)	K _L (L/mg)	R^2
10	41	1072	0.78	0.99	6.3	220	0.99
20	24	933	0.80	1.00	5.9	200	0.99
30	24	871	0.80	1.00	5.6	200	0.99
40	15	724	0.80	1.00	5.5	180	0.99
50	8	692	0.80	1.00	5.3	160	1.00

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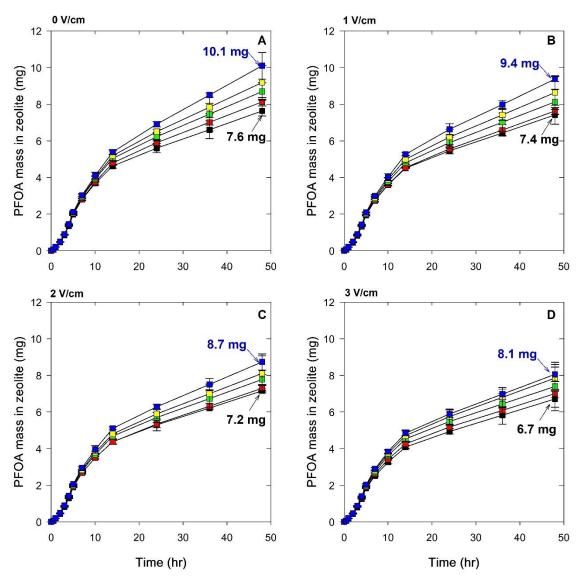


Figure 1. Perfluorooctanoic acid (PFOA) mass accumulated on zeolite under temperatures 10°C (blue), 20°C (yellow) 30°C (green), 40°C (red), and 50°C (black).

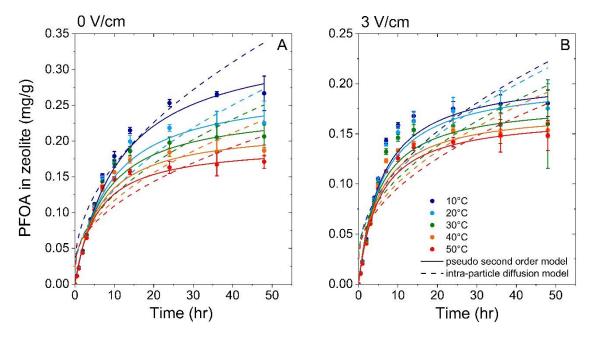


Figure 2. Effects of temperature ($T = 10 - 50^{\circ}$ C) on PFOA sorption kinetics DC field strengths of X = 0 (**Fig. 1A**) and 3 V/cm (**Fig. 1B**). The dashed and solid lines are the fitting curves of the intra-particle model and pseudo-second-order kinetic model, respectively.

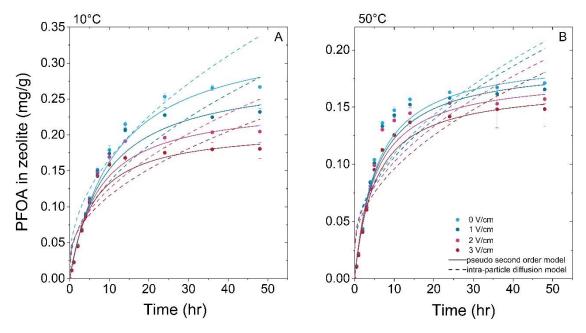


Figure 3. Effects of temperature ($T = 10^{\circ}$ C and 50° C) on sorption kinetics, with fitting curves of the intraparticle model and pseudo-second-order model, separately.

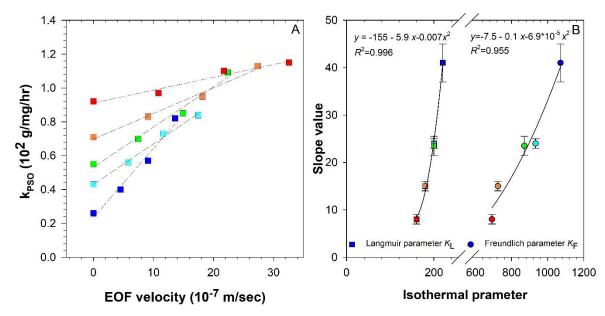


Figure 4. v_{EOF} correlation to the sorption kinetic constant (k_{PSO}) at $T = 10^{\circ}$ C (blue), 20°C (light blue), 30°C (green), 40°C (orange), 50°C (red) (**Fig. 4A**), and the derived slope values correlation with isothermal parameters (**Fig. 4B**).

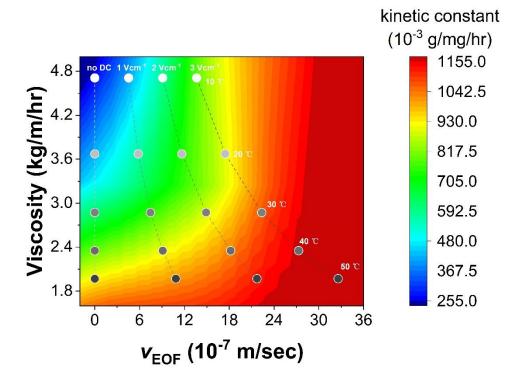


Figure 5. Interlinking between electroosmotic flow velocity ($v_{EOF, r}$), liquid viscosity (η), and their joint effects on PFOA sorption to zeolite. Warm colors reflect high k_{PSO} , i.e., decreased sorption, while cold colors reflect low k_{PSO} , i.e., increased sorption.