

$$\frac{dx(t)}{dt} = x(t) = I(t) \cdot b + x(t) \cdot re(t) \cdot A$$

## Name

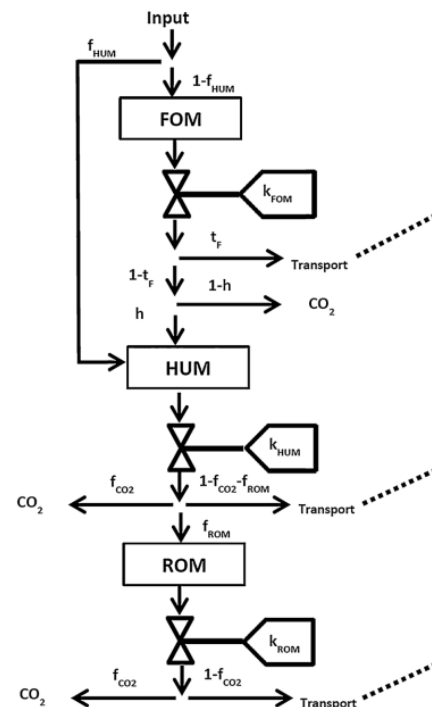
# C-Tool 2.3 (Topsoil)

## Important publications

(Taghizadeh-Toosi et al., 2014)

## Special features

- FOM gets only discriminated between Crop derived and Manure alike
- The model has no water dependency
- Modelling of subsoil is possible.



*pool concept (topsoil) of C-Tool (from Taghizadeh-Toosi et al., 2014)*

## Input distribution: b

Plant inputs enter completely into FOM. Manure (and other Amendments?) have a part that is directly put into HUM.  $b: (1-f_{HUM}, f_{HUM}, 0)^T$

$f_{HUM}: 0.358 - h$

$h: 1/(1.67 \cdot (1.85 + 1.6 \cdot e^{-7.86 \cdot clay}) + 1)$

## Initialisation: $x(t_0)$

Initial partition between HUM and ROM (top and sub soil) is set to HUM: 0.595, ROM: 0.405

## Environmental response: $re(t)$

$re(t)$  is only dependent on the monthly Temperature:

$$re(t) = 7.24 * e^{-3.432 + 0.168 \cdot \frac{1 - 0.5 \cdot T}{36.9}}$$

## Mass Flow Matrix: A

Flow rates are in  $[a^{-1}]$ . Rows are flows into each pool; columns are flows from each pool. Shown values are for pure sand.

For field experiments with no information about the subsoil, we assume the subsoil to be in steady-state, so that the flows into are the same as from it to  $CO_2$ . The amount and decay rates for the model pools are then the same, only the amount of  $CO_2$  might deviate from a model run with subsoil.

	$CO_2$	FOM_top	HUM_top	ROM_top
$CO_2$		1.233*	1.897e-2	4.63e-4
FOM_top		<b>-1.44</b>		
HUM_top		0.207*	<b>1.92e-2</b>	
ROM_top			0.023e-2	<b>-4.63e-4</b>

\*texture dependent

## References

Taghizadeh-Toosi, A., Christensen, B.T., Hutchings, N.J., Vejlin, J., Kätterer, T., Glendining, M., Olesen, J.E., 2014. C-TOOL: A simple model for simulating whole-profile carbon storage in temperate agricultural soils. *Ecol. Model.* 292, 11–25. <https://doi.org/10.1016/j.ecolmodel.2014.08.016>

## Additional info

For incubation-experiments, we argue that there is subsoil and so the flows to the subsoil are recycled:

	CO <sub>2</sub>	FOM_top	HUM_top	ROM_top
CO <sub>2</sub>		1.19*	1.206e-2	2.9e-4
FOM_top		<b>-1.397<sup>+</sup></b>		
HUM_top		0.207*	<b>1.229e-2</b>	
ROM_top			0.023e-2	<b>-2.9e-4</b>

\*texture dependent, <sup>+</sup>would probably be fitted

The whole pool structure would be:

	CO <sub>2</sub>	FOM_top	HUM_top	ROM_top	FOM_sub	HUM_sub	ROM_sub
CO <sub>2</sub>		$k \cdot 0.97 \cdot (1-h)$	$k \cdot f_{CO2}$	$k \cdot f_{CO2}$	$k \cdot 0.97 \cdot (1-h)$	$k \cdot f_{CO2}$	$k \cdot f_{CO2}$
FOM_top		<b>-1.44</b>					
HUM_top		$k \cdot (1-tf) \cdot h$	<b>-0.0192</b>				
ROM_top			$k \cdot f_{ROM}$	<b>-4.63e-4</b>			
FOM_sub		$k \cdot tf$			<b>-1.44 + k \cdot tf</b>		
HUM_sub			$k \cdot (1-f_{CO2} - f_{ROM})$		$k \cdot (1-tf) \cdot h$	<b>-0.0192</b>	
ROM_sub				$k \cdot (1-f_{CO2})$			<b>-4.63e-4</b> + $k \cdot (1-f_{CO2})$

tf (transport factor): 0.03,  $f_{CO2}$  (CO<sub>2</sub> factor for HUM and ROM): 0.628,  $f_{ROM}$  (transport from HUM to ROM): 0.012

h: partitioning of C from FOM to CO<sub>2</sub> and HUM. Dependent on the clay content:

$$h = 1 / (1.67 (1.85 + 1.60 \exp(-0.0786 \% \text{clay})) + 1)$$

Then h is formed HUM and (1-h) becomes CO<sub>2</sub>.